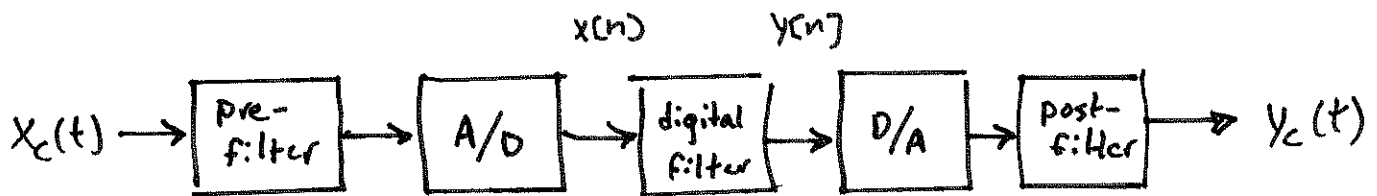


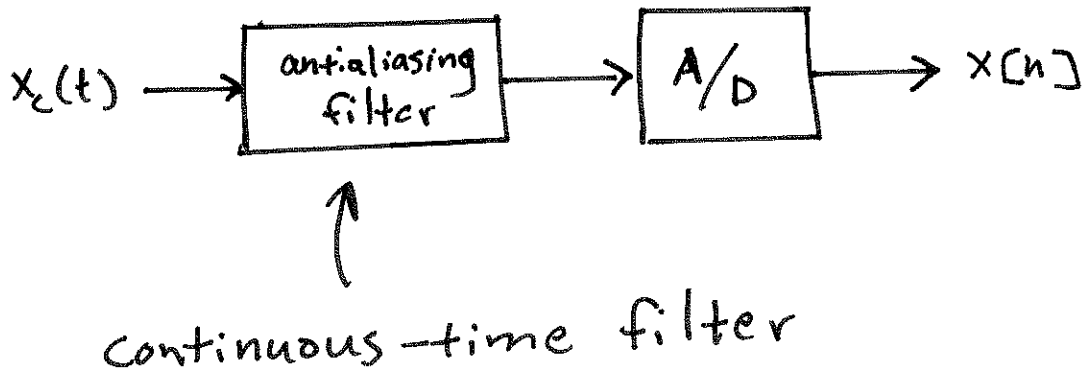
# Real-World DSP systems



## Practical Issues

1.  $x_c(t)$  bandlimited?
2. ideal lowpass filters?
3. ideal impulse trains?
4. quantization

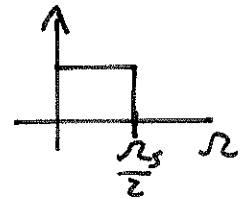
# Antialiasing Prefilter



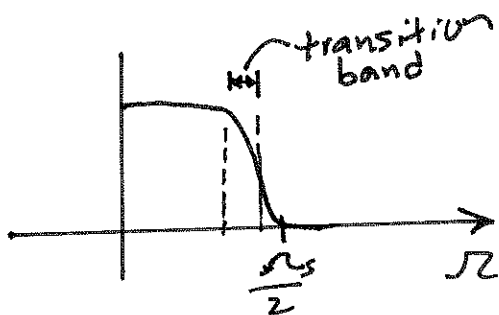
## Twofold Purpose:

1. bandlimits input signal  $x_c(t)$  to desired range (i.e.,  $|\Omega| \leq \Omega_s/2$ )
2. limits additive noise and other interference that may corrupt desired signal

Ideally: perfect lowpass filter

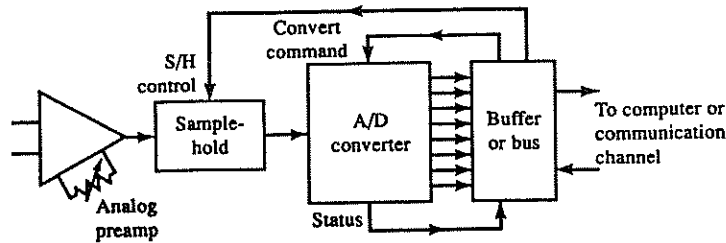
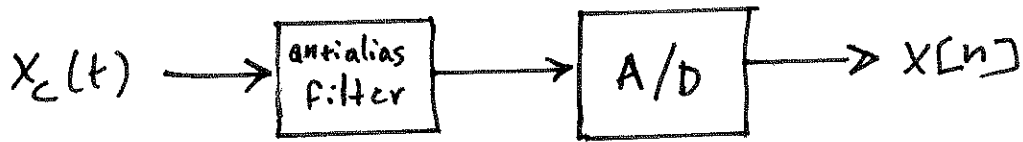


Practically: filter must be simple to implement in analog hardware



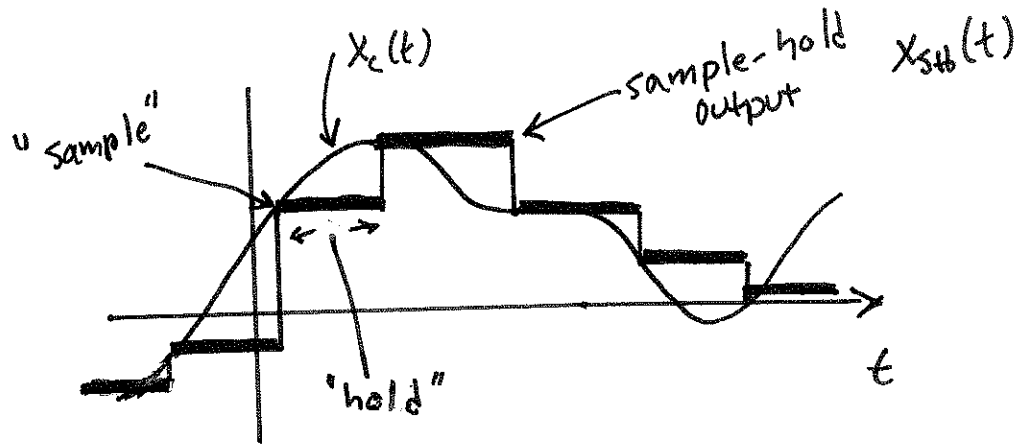
\* in practice we usually oversample signal so that the "sloppy" transition band doesn't hurt us.

# Analog-to-Digital Conversion



- non-ideal impulse sampling (sample-hold)
- quantization of real-valued current or voltage into a finite set of values or levels

# Sample-and-hold

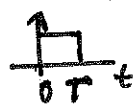


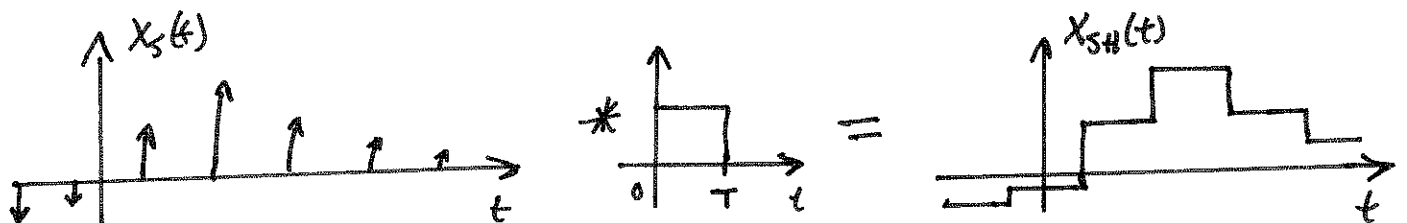
- "sample"  $x_c(t)$  <sup>once</sup> every  $T$  seconds

- "hold" voltage/current at sampled-value for  $T$  seconds

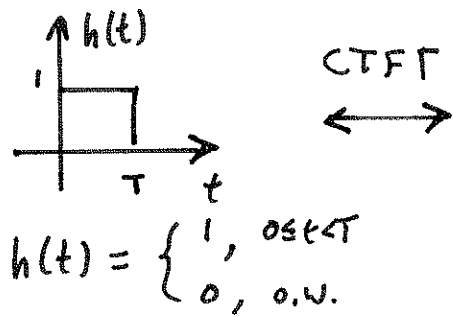
This is necessary so that the A/D converter circuitry has time to make the conversion

## Frequency Domain Interpretation:

Note sample-and-hold signal is effectively the ideal impulse sampled signal  $x_s(t)$  convolved with  - a short pulse of width  $T$



... in frequency

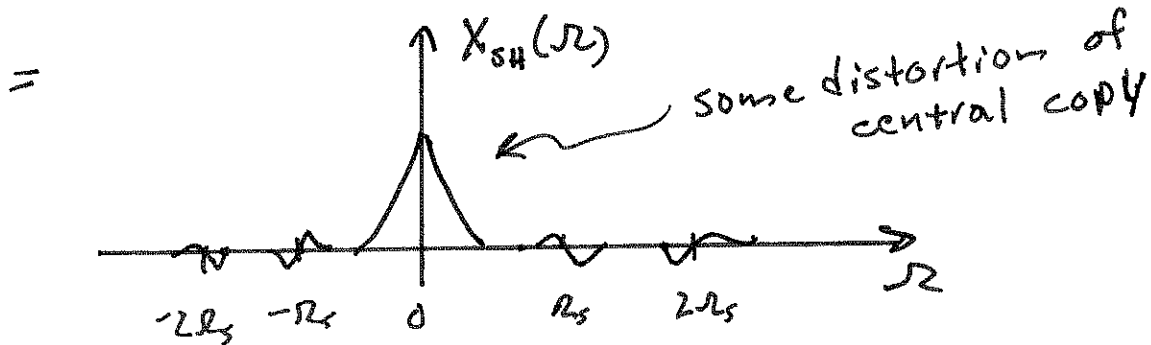
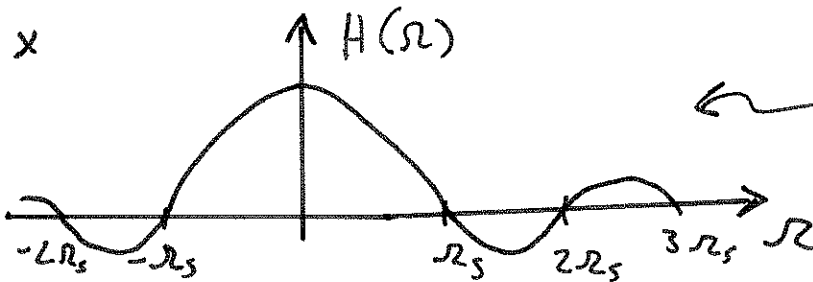
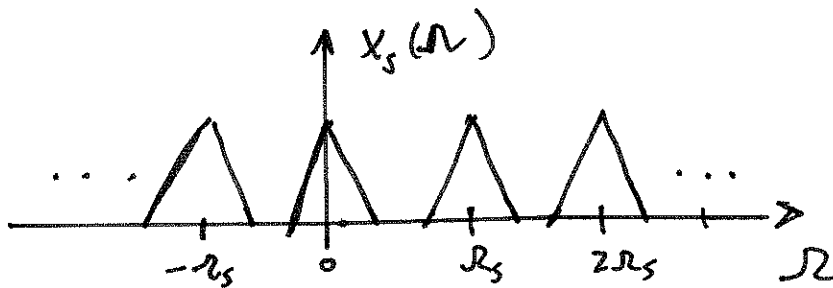


$$H(\Omega) = \int_{-\infty}^{\infty} h(t) e^{-j\Omega t} dt$$

$$= \int_0^T e^{-j\Omega t} dt$$

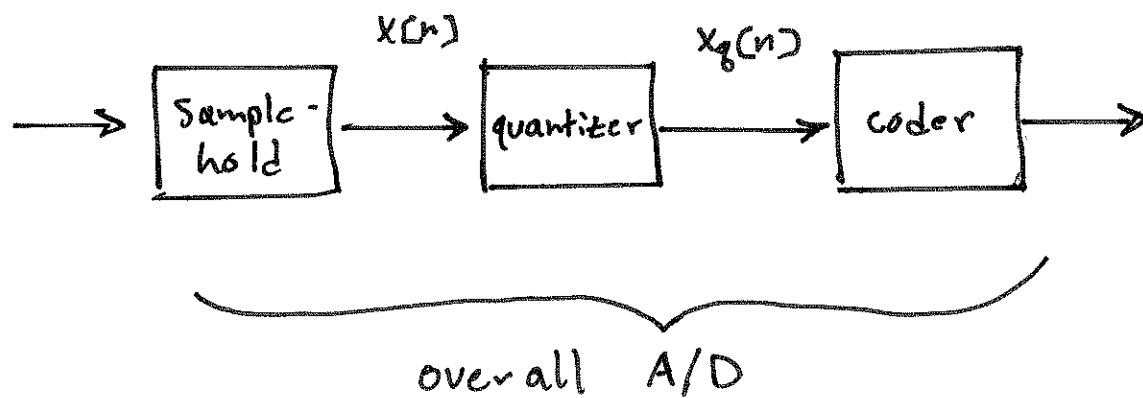
$$= e^{-j\frac{\Omega}{2}T} \underbrace{\frac{\sin \frac{\Omega}{2}T}{\frac{\Omega}{2}}}_{\text{Sinc}}$$

So,



How can this distortion be minimized?

# Quantization & Coding



Let  $x(n) \equiv x(nT)$  as before.

Suppose that  $x(n)$ 's amplitude range is known (and limited).

Divide signal's amplitude range into  $L$  intervals:

$$I_k = \{ a_k < x(n) < a_{k+1} \}$$
$$k = 1, 2, \dots, L$$

where  $a_1, \dots, a_{L+1}$  are the decision levels.

The possible outputs of the quantizer  
( quantization levels ) are denoted

$$\hat{x}_1, \hat{x}_2, \dots, \hat{x}_L.$$

The operation of the quantizer  
is defined as

$$x_q[n] = Q(x[n]) = \hat{x}_k$$

$$\text{if } x[n] \in I_k$$

$$\text{(i.e., } x_k < x[n] \leq x_{k+1} \text{)}$$

In most DSP systems

1. Q is memoryless

- quantization of  $x[n]$  depends  
only on that sample, no others

- quantization operation is  
independent of  $n$  (time-invariant)

2. Q is uniform

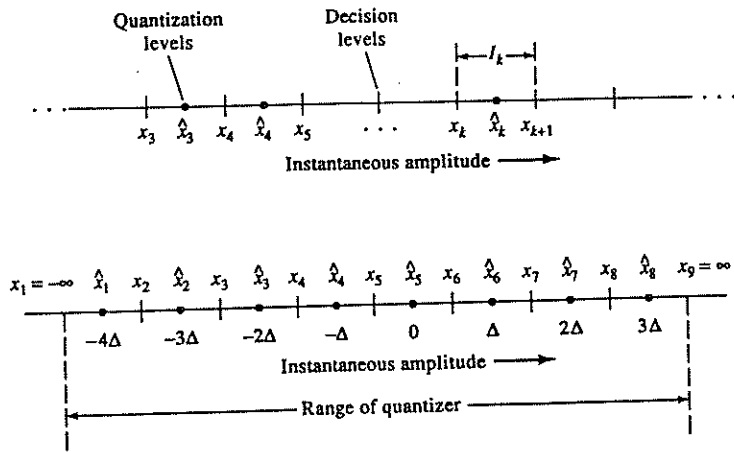
$$\hat{x}_{k+1} - \hat{x}_k = \Delta$$

$$x_{k+1} - x_k = \Delta$$

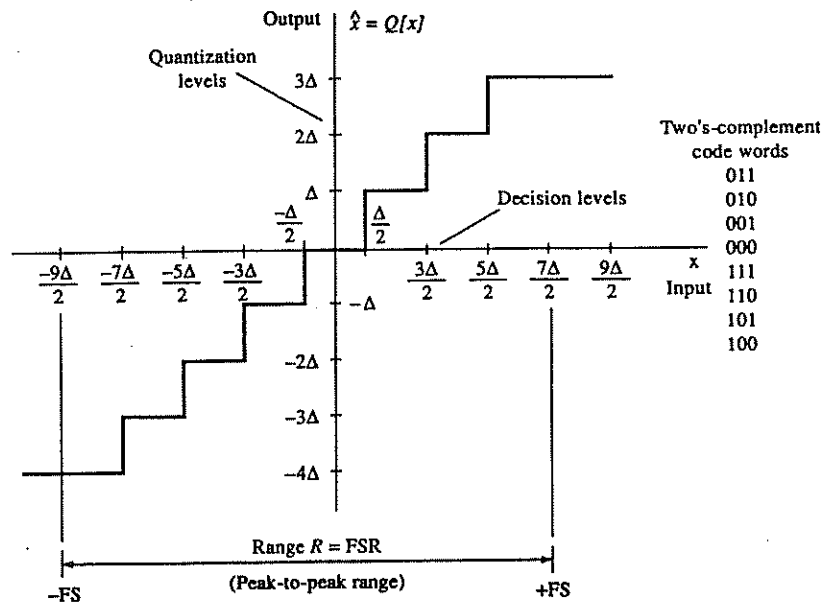
$\Delta =$  quantization  
step size

"uniform quantizer"

# Quantization process:



# I/O Relationship:





## Quantization Error:

$$e_q[n] = x[n] - x_q[n]$$

Note

$$-\frac{\Delta}{2} < e_q[n] \leq \frac{\Delta}{2}$$

## Coding:

Assigns a unique binary number to each quantization level.

If we have  $L$  levels, then we need at least  $L$  different binary numbers.

Using  $b+1$  bit word-length provides us with  $2^{b+1}$  binary numbers or codes.

Hence, we require

$$2^{b+1} \geq L \quad \text{or} \quad b+1 \geq \log_2 L$$

With a  $(b+1)$  length coding scheme,  
the step size or resolution of  
the A/D converter is

$$\Delta = \frac{R}{2^{b+1}}$$

Where  $R$  is the range of the  
quantizer.

Commonly Used Bipolar Codes

Number	Decimal Fraction		Sign + Magnitude	Two's Complement	Offset Binary	One's Complement
	Positive Reference	Negative Reference				
+7	$+\frac{7}{8}$	$-\frac{7}{8}$	0111	0111	1111	0111
+6	$+\frac{6}{8}$	$-\frac{6}{8}$	0110	0110	1110	0110
+5	$+\frac{5}{8}$	$-\frac{5}{8}$	0101	0101	1101	0101
+4	$+\frac{4}{8}$	$-\frac{4}{8}$	0100	0100	1100	0100
+3	$+\frac{3}{8}$	$-\frac{3}{8}$	0011	0011	1011	0011
+2	$+\frac{2}{8}$	$-\frac{2}{8}$	0010	0010	1010	0010
+1	$+\frac{1}{8}$	$-\frac{1}{8}$	0001	0001	1001	0001
0	0+	0-	0000	0000	1000	0000
0	0-	0+	1000	(0000)	(1000)	1111
-1	$-\frac{1}{8}$	$+\frac{1}{8}$	1001	1111	0111	1110
-2	$-\frac{2}{8}$	$+\frac{2}{8}$	1010	1110	0110	1101
-3	$-\frac{3}{8}$	$+\frac{3}{8}$	1011	1101	0101	1100
-4	$-\frac{4}{8}$	$+\frac{4}{8}$	1100	1100	0100	1011
-5	$-\frac{5}{8}$	$+\frac{5}{8}$	1101	1011	0011	1010
-6	$-\frac{6}{8}$	$+\frac{6}{8}$	1110	1010	0010	1001
-7	$-\frac{7}{8}$	$+\frac{7}{8}$	1111	1001	0001	1000
-8	$-\frac{8}{8}$	$+\frac{8}{8}$		(1000)	(0000)	

Two's complement is the most common representation in most processors, so it's convenient to adopt this coding scheme in A/D conversion.

## Two's Complement Representation

(b+1)-bit code:  $\beta_0 \beta_1 \dots \beta_b$  ← LSB = least significant bit

Value:  $-\beta_0 2^0 + \beta_1 2^{-1} + \beta_2 2^{-2} + \dots + \beta_b 2^{-b}$

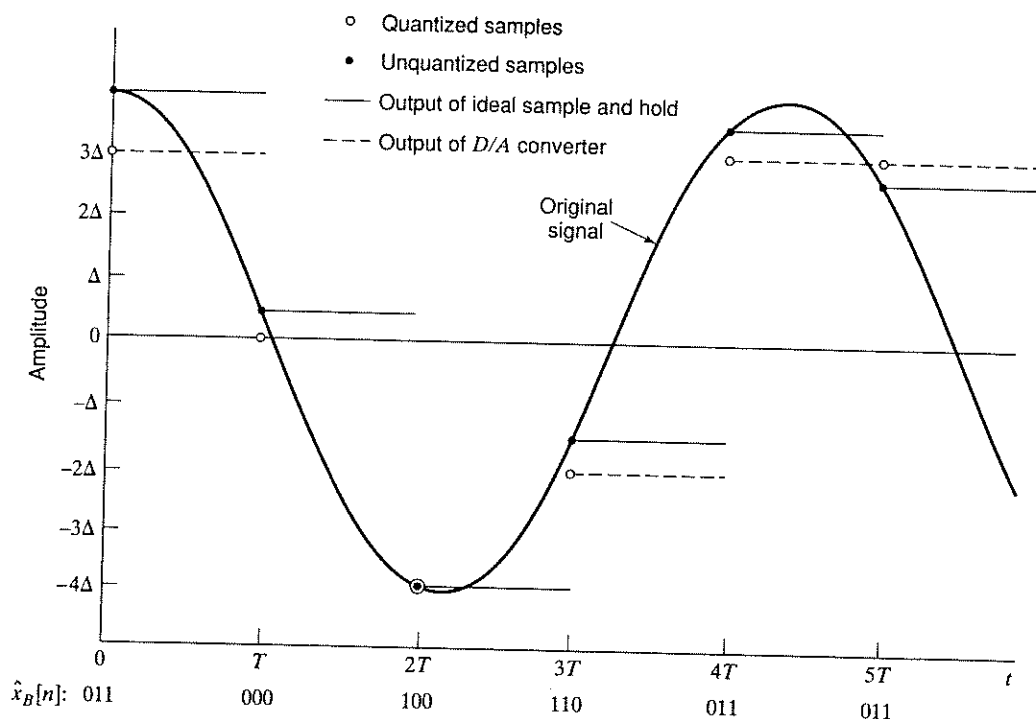


Figure 4.49 Sampling, quantization, coding, and D/A conversion with a 3-bit quantizer.

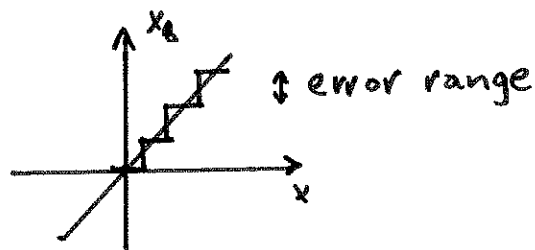
# Analysis of Quantization Errors

Worst case:  $\max |x[n] - x_q[n]| = \frac{\Delta}{2}$

$\underbrace{\hspace{10em}}_{e_q[n]}$

Most errors fall somewhere in between

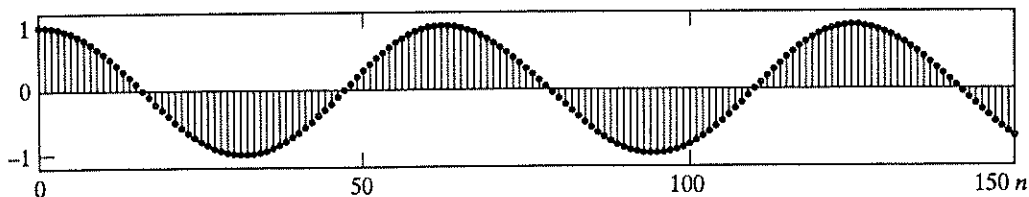
$$0 \leq |e_q[n]| \leq \frac{\Delta}{2}$$



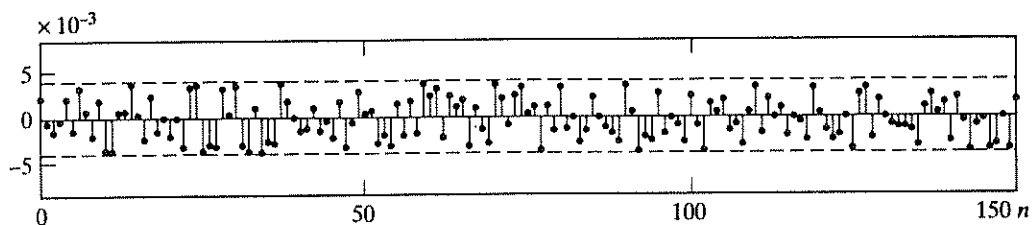
The error between  $x[n]$  and  $x_q[n]$  is referred to as granular noise.

Ex.

Sinusoidal  
input  
 $x[n]$



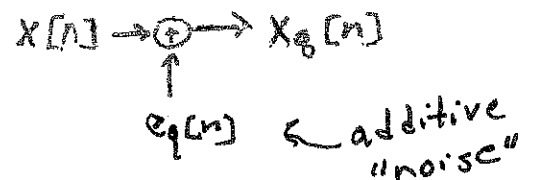
$e_q[n] =$   
 $x[n] - x_q[n]$



# Statistical Analysis of Granular Noise

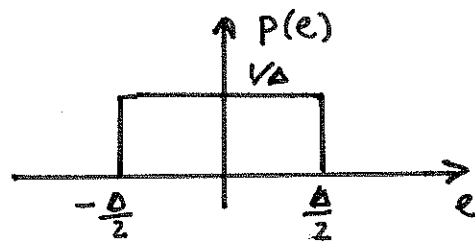
Because, of the complicated nature of quantization errors, it can be useful to regard the granular noise as a random process (instead of a deterministic one).

Is this reasonable?



## Assumptions:

1.  $e_q[n]$  is a realization of a stationary (wide-sense) random process
2.  $e_q[n]$  is uniformly distributed over  $(-\frac{\Delta}{2}, \frac{\Delta}{2}]$



and zero-mean

3.  $e_q[n]$  is an uncorrelated process (white noise)
4.  $e_q[n]$  is independent of  $x[n]$ , also a WSS process.

★ These assumptions do not hold, in general. However, if the quantization step size  $\Delta$  is small enough, then the signal sequence  $x[n]$  traverses several quantization levels between successive samples and 1-4 are reasonable.

## Signal-to-Quantization Noise Ratio (SQNR)

$$\text{SQNR} = 10 \log_{10} \frac{\sigma_x^2}{\sigma_e^2} \quad (\text{dB})$$

$$\sigma_x^2 = E[x^2[n]]$$

$$\sigma_e^2 = E[e_q^2[n]]$$

$$= \int_{-\frac{A}{2}}^{\frac{A}{2}} e^2 p(e) de$$

$$\text{SQNR} = 10 \log_{10} \left( 12 \frac{\sigma_x^2}{\Delta^2} \right)$$

Now recall,

$$\Delta = \frac{R}{2^{b+1}}$$

$$\text{SQNR} = 10 \log_{10} \left( 12 \frac{\sigma_x^2 (2^{b+1})^2}{R^2} \right)$$

$$= 20 \log_{10} (2^{b+1}) + 10 \log_{10} (12) - 20 \log_{10} \left( \frac{R}{\sigma_x} \right)$$

$$= 6.02 b + 16.81 - 20 \log_{10} \left( \frac{R}{\sigma_x} \right)$$

↗  
depends on  $R$  (range)  
and statistics of  $X[n]$

Suppose that  $X[n]$  is a stationary Gaussian process and that the quantizer range is

$$R = [-3\sigma_x, +3\sigma_x].$$

Then less than 3 out of every 1000 samples would fall out of the range on average, and

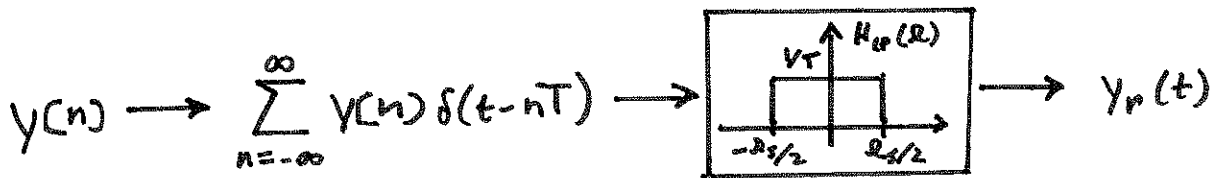
$$\boxed{\text{SQNR} \approx 6.02b + 1.25 \text{ dB}}$$

↖ commonly used to specify precision needed in A/D converters

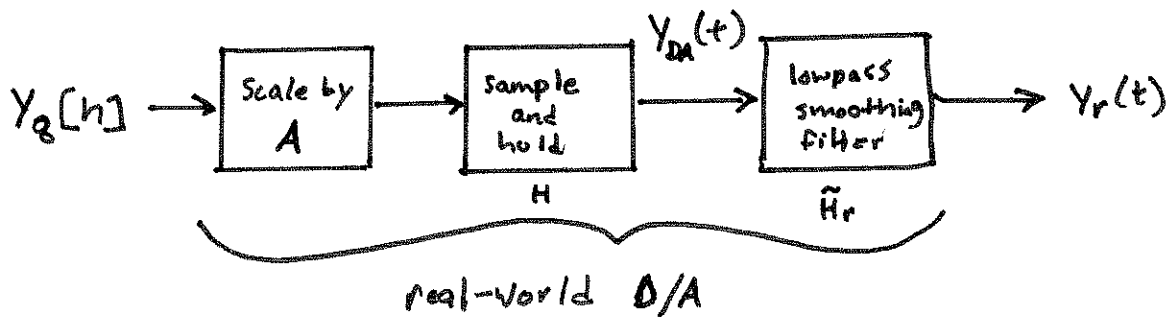
# Digital-to-Analog Conversion

Ideal:

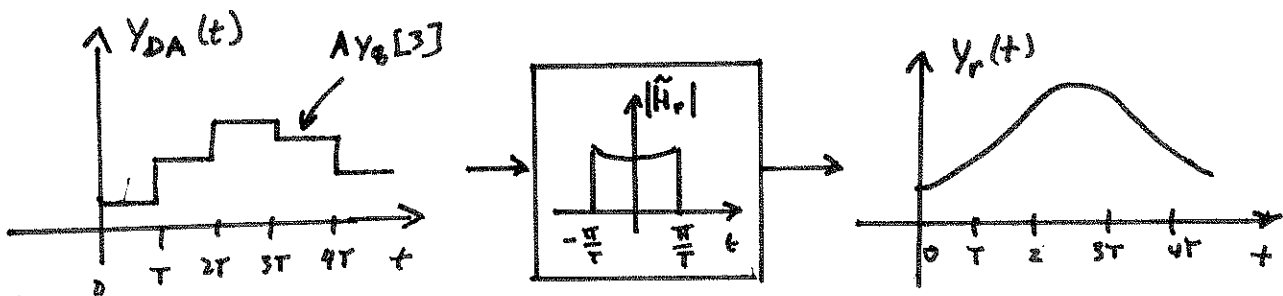
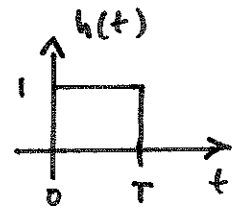
$$Y_r(t) = \sum_{n=-\infty}^{\infty} Y[n] \frac{\sin[\pi(t-nT)/T]}{\pi(t-nT)/T}$$



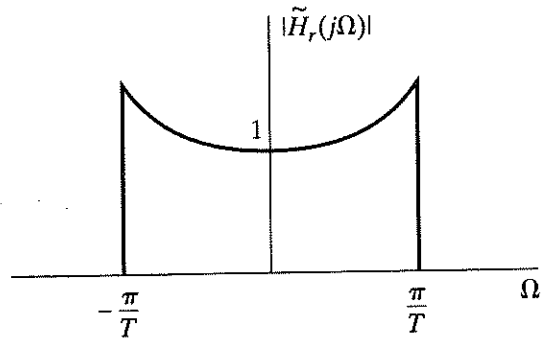
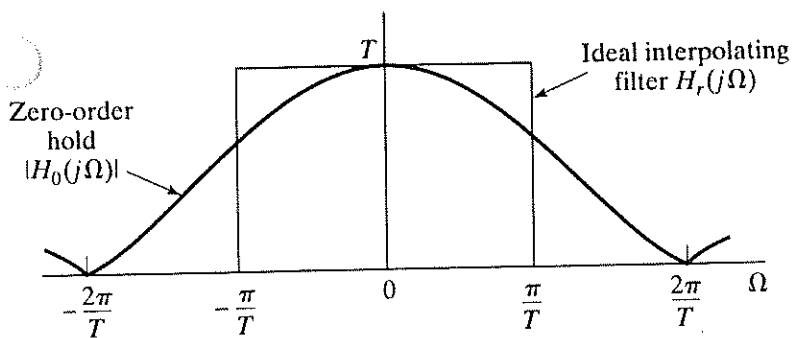
## Real-World Reconstruction Using Sample-and-Hold:



$$Y_{DA}(t) = \sum_{n=-\infty}^{\infty} A Y_Q[n] h(t-nT)$$







## DSP System Analysis



$$e_g'[n] = \sum_{k=-\infty}^{\infty} g[k] e_g[n-k]$$

$$S_{ee}(w) =$$

$$\Rightarrow S_{e'e'}(w) =$$

SET F:

The z-transform

## OSB Chapter 3

### Outline

I. z-transform

II. Properties and ROC

III. Inverse z-Transform

IV. z-Transform Analysis  
of LTI Systems and Filters

# A Brief intro to filter design

An FIR (finite impulse response) filter takes the form



$$y[n] = \sum_{k=0}^{M-1} h[k] x[n-k]$$

The frequency response of an FIR filter is given by its DTFT

$$H(\omega) = \sum_{k=0}^{M-1} h[k] e^{-j\omega k}$$

FIR filters are just one type of a more general class of realizable DSP filters known as linear, constant-coefficient difference equations (LCCDEs).

The general form of an LCCDE is

$$y[n] = \sum_{k=1}^N a_k y[n-k] + \sum_{k=0}^M b_k x[n-k]$$

Note that this type of filter is IIR (infinite impulse response) in general, but also includes FIR filters ( $a_k=0, k=1, \dots, N$ ).

What is the frequency response of an LCCDE?

$$y[n] = \sum_{k=1}^N a_k y[n-k] + \sum_{k=0}^M b_k x[n-k]$$

$$Y(\omega) =$$

# I. The z-Transform

What is it?

1. Counterpart of the LAPLACE TRANSFORM for DT signals and systems

2. A Generalization of the DTFT

Why generalize the DTFT?

- Because the DTFT doesn't exist (i.e., converge) for many important signals.
- Notationally cleaner than DTFT (easy to work with).
- Brings the power of complex variable theory to bear on DSP.

$$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$$

$z \in \mathbb{C}$

↓  
set of complex numbers

# The Z-Transform

A generalization of the DTFT:

DTFT:  $X(\omega) = \sum_{n=-\infty}^{\infty} x[n] e^{-j\omega n}$

Complex number  
 $|e^{-j\omega n}| = 1$

Z-transform:  $X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$

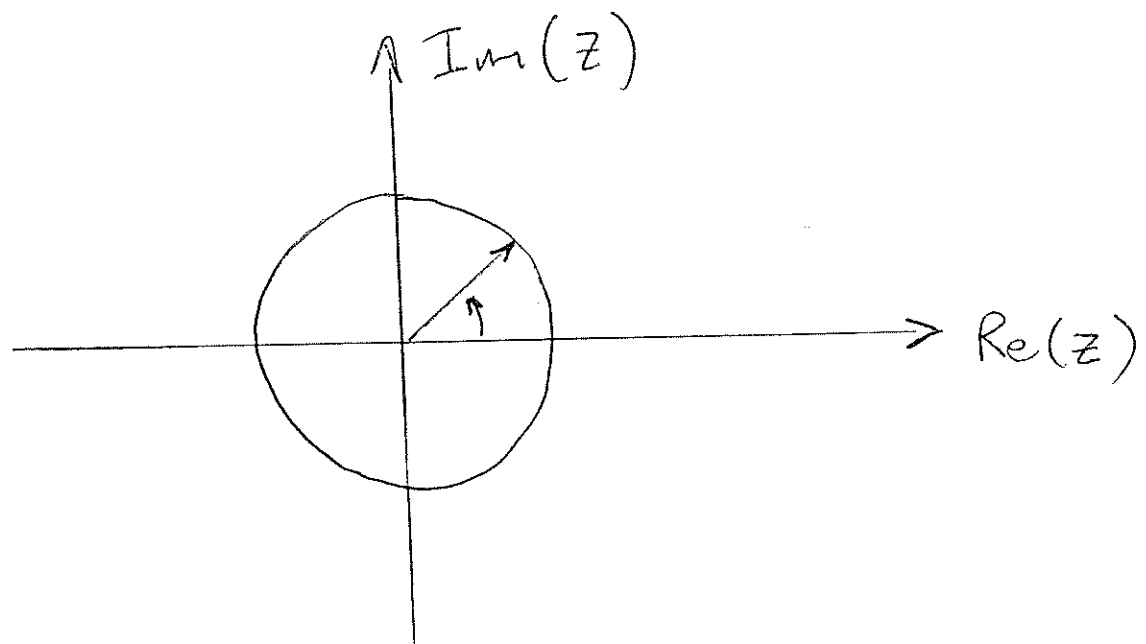
general complex number  
 $|z| \in \mathbb{R}$

Note:  
 $X(\omega) = X(z) \Big|_{z=e^{j\omega}}$

★ DTFT is a complex-valued function of a real-valued variable

★ Z-Transform is a complex-valued function of a complex-valued variable  $z$ .

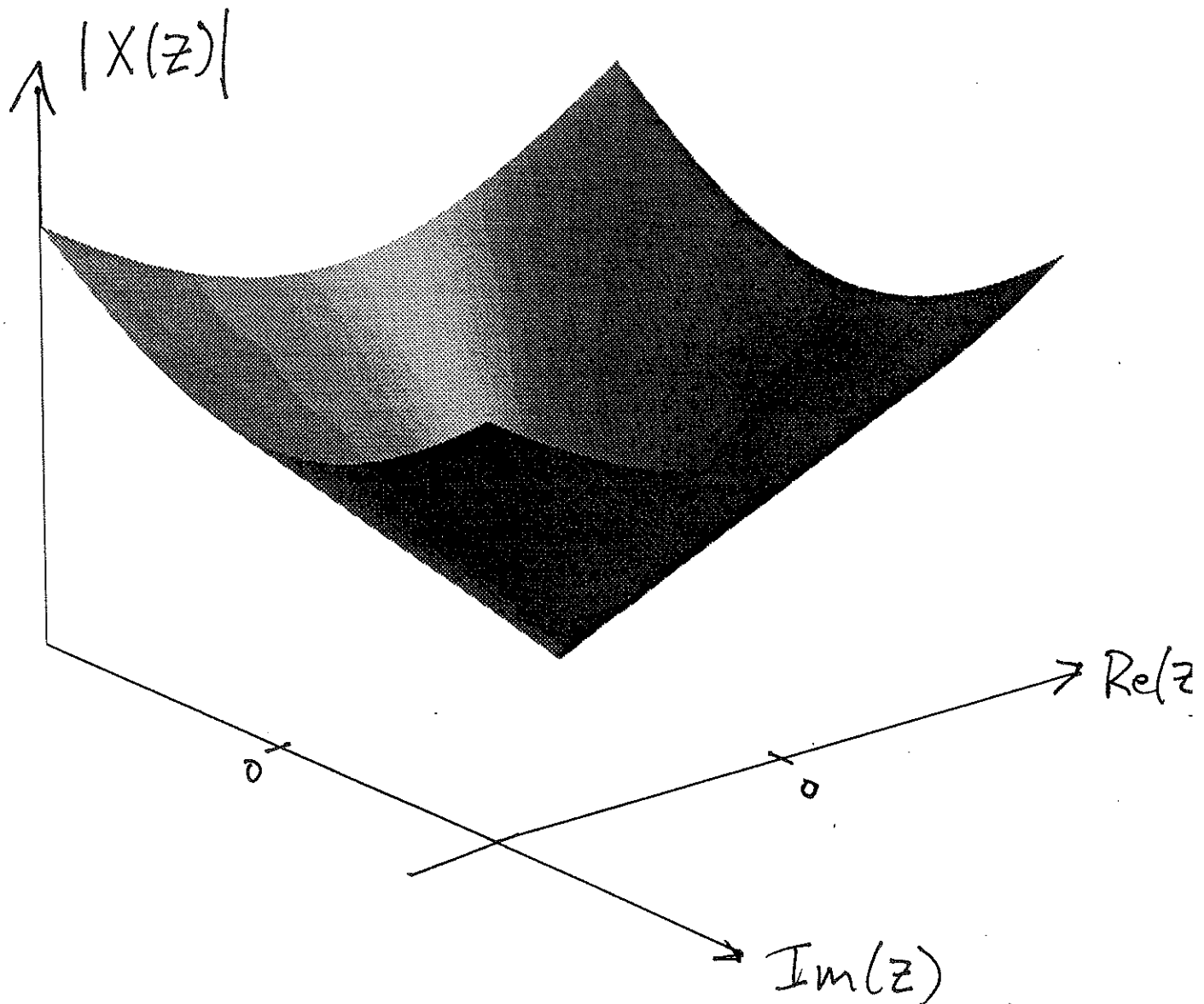
# The Complex Plane (The $z$ -plane)



- $X(z)$  is defined everywhere on this plane
- $X(w)$  is defined only on the unit circle



ex.  $X(z) = z$



It's a cone!

What is the DTFT in this case?

Ex. Sketch  $X(z) = \frac{z}{z-a}$

Note: The DTFT corresponds to the evaluation of the z-Transform on the unit circle

⇒ Periodicity of  $X(\omega)$  becomes obvious

We write:

$$\mathcal{Z} \{ x[n] \} = X(z) \quad \text{"z-Transform operator"}$$

$$x[n] \xleftrightarrow{\mathcal{Z}} X(z)$$

Ex.  $x[n] = \delta[n - n_0]$  delay

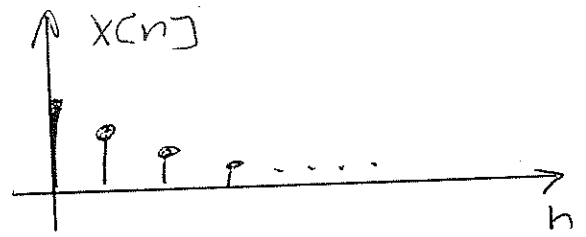
$$\begin{aligned} X(z) &= \sum_{n=-\infty}^{\infty} x[n] z^{-n} \\ &= \sum_{n=-\infty}^{\infty} \delta[n - n_0] z^{-n} = z^{-n_0} \end{aligned}$$

$$\boxed{X(z) = z^{-n_0}}$$

$n_0 = 1 \rightarrow X(z) = z^{-1}$  (unit delay in z-Transform Domain)

Example: Let's look at

$$x[n] = \alpha^n u[n]$$



$$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$$

$$= \sum_{n=0}^{\infty} \alpha^n z^{-n} = \sum_{n=0}^{\infty} (\alpha z^{-1})^n$$

$$= \frac{1}{1 - \alpha z^{-1}} \quad \left( \text{if } |\alpha z^{-1}| < 1 \right)$$

$$X(z) = \frac{z}{z - \alpha}$$

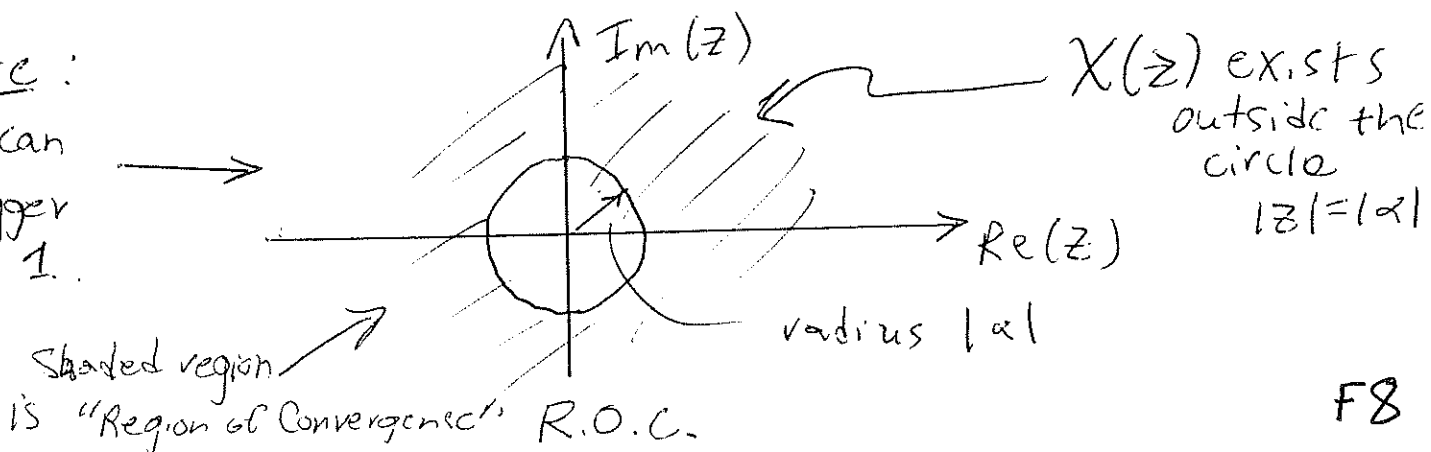
What if  $|\alpha z^{-1}| \geq 1$ ?

Then  $\sum_{n=0}^{\infty} (\alpha z^{-1})^n$  does not converge!

Therefore we must specify the set of  $z$ 's for which the  $z$ -transform exists.

$$|\alpha z^{-1}| < 1 \rightarrow |z| > |\alpha|$$

Note:  
 $|\alpha|$  can  
be bigger  
than 1.



Ex. "The evil twin"

$$x_2[n] = -\alpha^n u[-1-n]$$

$$\begin{pmatrix} -1-n \geq 0 \\ \rightarrow n \leq -1 \end{pmatrix}$$



$$\begin{aligned} X_2(z) &= \sum_{n=-\infty}^{\infty} x_2[n] z^{-n} \\ &= \sum_{n=-\infty}^{-1} -\alpha^n z^{-n} \\ &= \sum_{n=-\infty}^{-1} -(\alpha^{-1} z)^{-n} \\ &= -\sum_{n=1}^{\infty} (\alpha^{-1} z)^n \end{aligned}$$

$$|\alpha^{-1} z| < 1 \rightarrow X_2(z) = -\sum_{n=0}^{\infty} (\alpha^{-1} z)^n + 1$$

$$= \frac{1}{-1 + \alpha^{-1} z} + 1$$

$$= \frac{\alpha}{z - \alpha} + 1$$

$$= \frac{\alpha + z - \alpha}{z - \alpha} = \frac{z}{z - \alpha}$$

Non-uniqueness of z-transforms!

# Region of Convergence

Clearly The region where  $X(z)$  exists is pretty important.

Defn: For a given signal  $x[n]$ , the range of  $z$  for which the  $z$ -transform converges is called the ROC.

$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$  is a power series that converges when  $x[n] z^{-n}$  is abs. summ.

i.e.,

$$\sum_{n=-\infty}^{\infty} |x[n] z^{-n}| = \sum_{n=-\infty}^{\infty} |x[n]| |z|^{-n} < \infty$$

e.g. ROCs of  $\sum \alpha^n u[n]$   
and  $\sum -\alpha^n u[-1-n]$  are drastically different.

# Poles & Zeros

Among the most useful & important z-transforms are

Rational Functions  $X(z) = \frac{P(z)}{Q(z)}$

with  $P(z)$  and  $Q(z)$  polynomials in  $z$

Zeros: Values of  $z$  for which  $X(z) = 0$   
( $P(z) = 0$ )

Poles: Values of  $z$  for which  $X(z) = \infty$   
( $Q(z) = 0$ )

- For finite values of  $z$ , poles are the roots of  $Q(z)$
- In addition, poles may occur at  $z = 0$  or  $z = \infty$

We denote poles in a z-plane plot by "x"

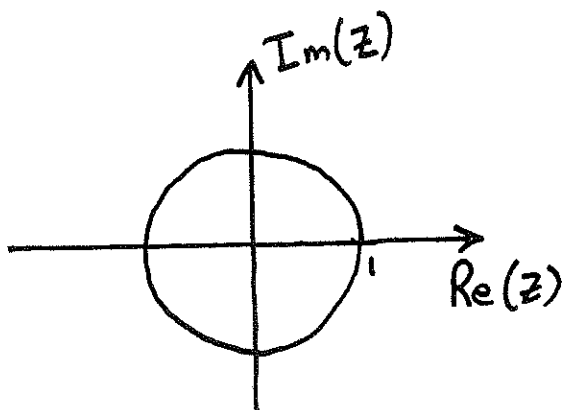
We denote zeros by "o"

\* Clearly the ROC cannot contain any poles. Why?

Ex.

$$X_1[n] = \alpha^n u[n] \xleftrightarrow{Z} X_1(z) = \frac{z}{z-\alpha}$$

$$|z| > |\alpha|, \quad |\alpha| < 1$$

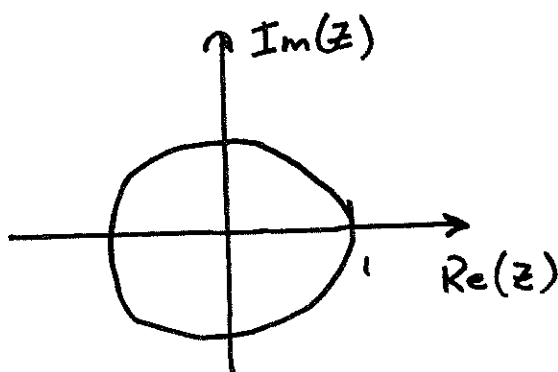


zero:

pole:

$$X_2[n] = -\alpha^n u[-1-n] \xleftrightarrow{Z} X_2(z) = \frac{z}{z-\alpha}$$

$$|z| < |\alpha| < 1$$



zero:

pole:

Note: Both  $X_1(z) \stackrel{!}{\neq} X_2(z)$  are rational

Note: the z-transform is linear:

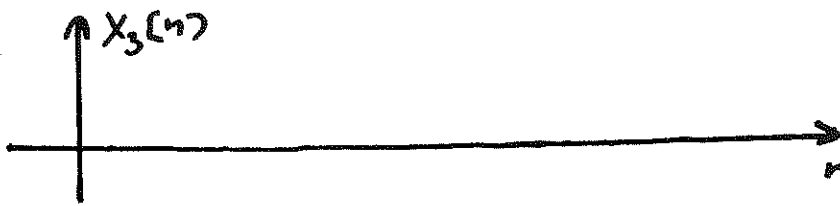
$$y[n] = x_1[n] + x_2[n]$$

$$Y(z) = \sum_n y[n] z^{-n} =$$

=

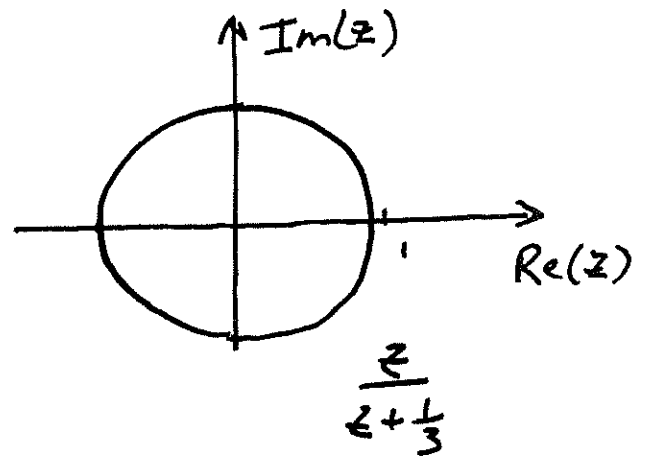
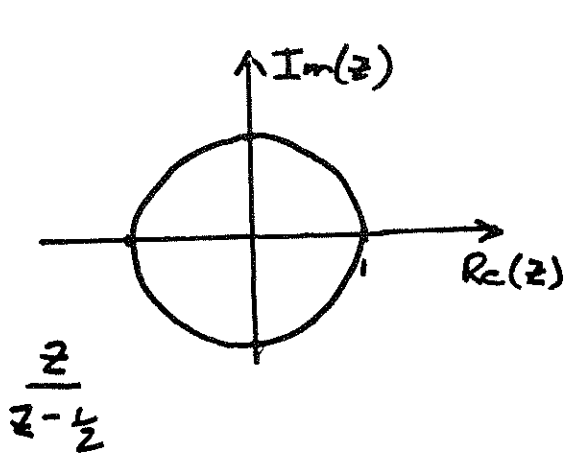


Ex.  $X_3[n] = \left(\frac{1}{2}\right)^n u[n] + \left(-\frac{1}{3}\right)^n u[n]$



$\left(\frac{1}{2}\right)^n u[n] \xleftrightarrow{Z} \frac{z}{z - \frac{1}{2}}$       ROC: \_\_\_\_\_

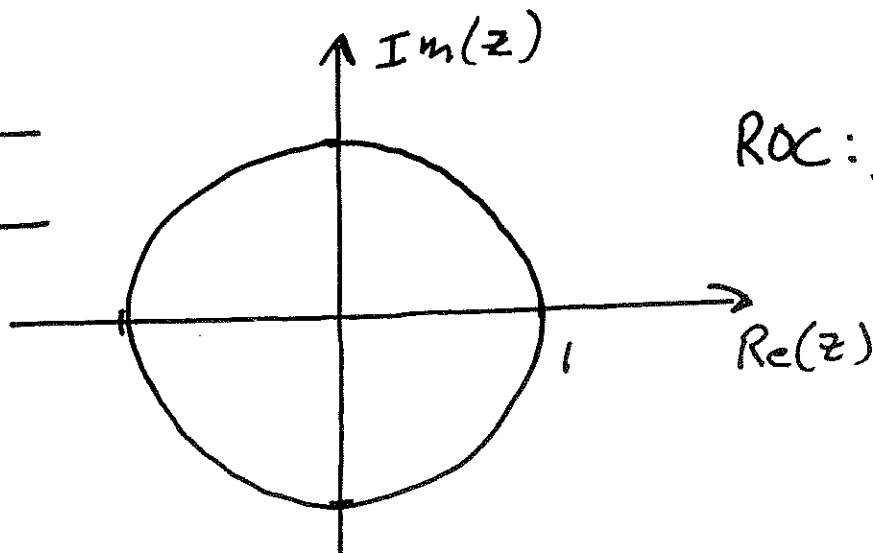
$\left(-\frac{1}{3}\right)^n u[n] \xleftrightarrow{Z} \frac{z}{z + \frac{1}{3}}$       ROC: \_\_\_\_\_



Linearity  $\Rightarrow X_3(z) = \frac{z}{z - \frac{1}{2}} + \frac{z}{z + \frac{1}{3}} = \frac{z(2z - \frac{1}{6})}{(z - \frac{1}{2})(z + \frac{1}{3})}$

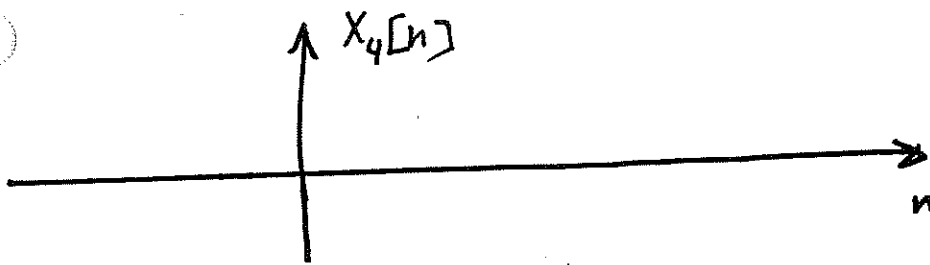
Zeros: \_\_\_\_\_

Poles: \_\_\_\_\_



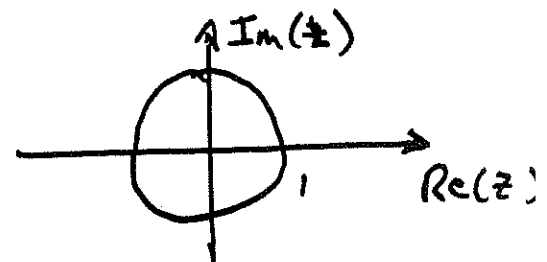
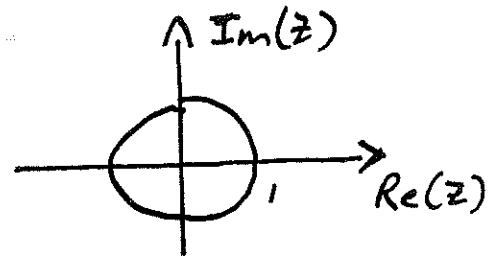
ROC: \_\_\_\_\_

Ex.  $X_4[n] = \left(-\frac{1}{3}\right)^n u[n] - \left(\frac{1}{2}\right)^n u[-n-1]$



$\left(-\frac{1}{3}\right)^n u[n] \xleftrightarrow{z}$

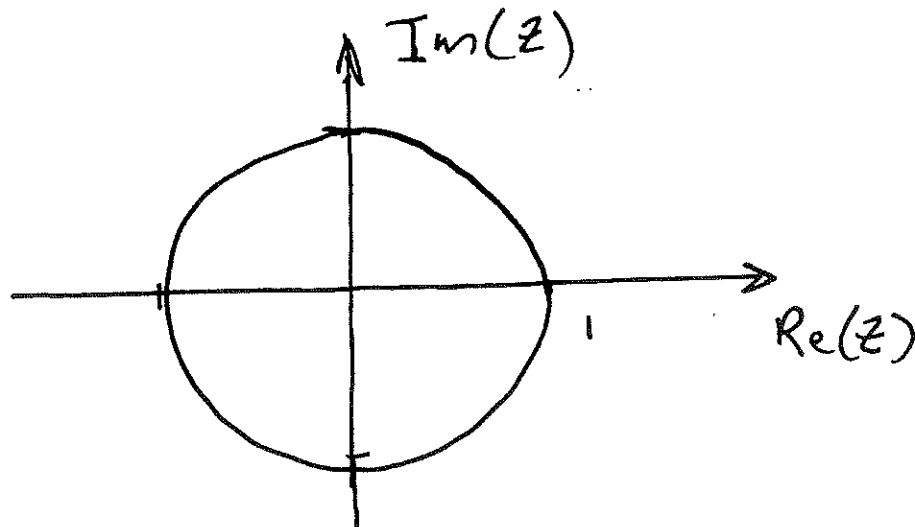
$-\left(\frac{1}{2}\right)^n u[-n-1] \xleftrightarrow{z}$



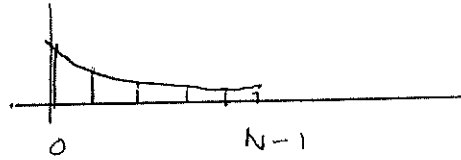
So, by linearity

$X_4(z) =$

ROC: \_\_\_\_\_



Ex.  $X[n] = \begin{cases} \alpha^n, & 0 \leq n \leq N-1 \\ 0, & \text{o.w.} \end{cases}$



$$X(z) = \sum_{n=0}^{N-1} X[n] z^{-n} = \sum_{n=0}^{N-1} (\alpha z^{-1})^n$$

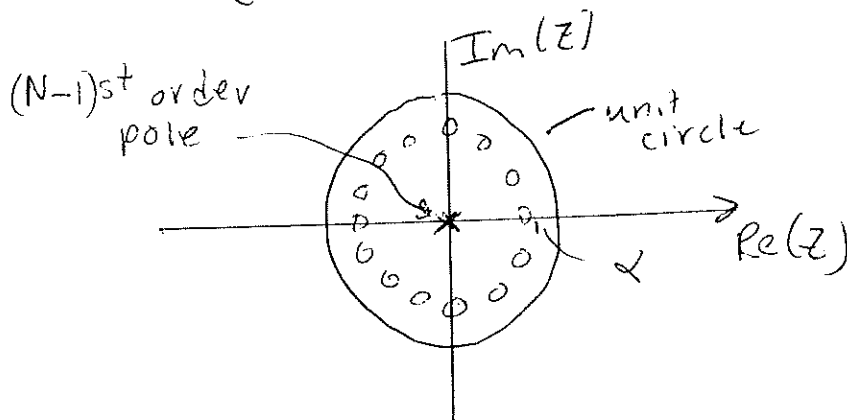
$$= \frac{1 - (\alpha z^{-1})^N}{1 - \alpha z^{-1}} = \frac{1}{z^{N-1}} \frac{z^N - \alpha^N}{z - \alpha}$$

ROC:  $\sum_{n=0}^{N-1} |\alpha z^{-1}|^n < \infty \iff |\alpha| < \infty, \neq |z| \neq 0$

So, if  $|\alpha| < \infty$ , ROC is the entire  $z$ -plane except origin.

Zeros:  $z^N = \alpha^N \rightarrow z_k = \alpha e^{j \frac{2\pi}{N} k}$   
 $\nearrow k=0, 1, \dots, N-1$   
 "N<sup>th</sup> root of unity"

poles:  $z=0$  (N-1 of them) +  ~~$z=\alpha$~~  cancelled by a zero at  $\alpha$



# Inverse Z-transform

$$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$$

Question: Given  $X(z)$ , how can we find  $x[n]$ ?

Inverting the Z-transform is different from inverting, say, the DTFT.

We'll look at four methods:

- a. Inspection
  - b. Partial Fraction Expansion
  - c. Power series Expansion
  - d. Contour Integration
- } "tables"

## (a) Inspection

Basically, become familiar with the  $z$ -transform pair tables and "reverse engineer"

ex.  $X(z) = \frac{z}{z-a}, |z| > |a|$

↑ "looks mighty familiar"

Looking in tables gives  $x[n] = a^n u[n]$ .

## (b) Partial Fractions Expansion

Basically this: Break a rational  $X(z)$  up into elementary forms, each of which can be inverse transformed "by inspection"

Ex.  $X(z) = \frac{1 + 2z^{-1} + z^{-2}}{1 - \frac{3}{2}z^{-1} + \frac{1}{2}z^{-2}} = \frac{8}{1-z^{-1}} - \frac{9}{1-\frac{1}{2}z^{-1}} + 2$

$|z| > 1$

easy to invert!

PF expansion

★ PF expansion always works for rational functions

★★ Review / Relearn how to do PF

### Partial Fractions

$$\text{Given } X(z) = \frac{\sum_{k=0}^m b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}} \quad \text{rational in } z^{-1}$$

Note: We can express this as

$$X(z) = \frac{b_0}{a_0} \frac{\prod_{k=1}^m (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

$\{c_k\}$  - nonzero zeros of  $X(z)$

$\{d_k\}$  - nonzero poles of  $X(z)$

We would like to express  $X(z)$  as a sum in terms of the form

$$\frac{A_k}{1 - d_k z^{-1}} \quad \leftarrow \text{can be inverted "by inspection"}$$

STEP 1: If  $M \geq N$ , divide numerator by denominator to get

$$X(z) = \sum_{r=0}^{M-N} B_r z^{-r} + \frac{\sum_{k=0}^{N-1} b'_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

eg.  $X(z) = \frac{1 + 2z^{-1} + z^{-2}}{1 - \frac{3}{2}z^{-1} + \frac{1}{2}z^{-2}} \quad \begin{matrix} \curvearrowright \\ \Rightarrow \end{matrix} \begin{matrix} M=N=2 \\ \text{Have to} \\ \text{divide} \end{matrix}$

$$\frac{1}{2} z^{-2} - \frac{3}{2} z^{-1} + 1 \quad \begin{matrix} \sqrt{2} \\ \text{long} \\ \text{division} \end{matrix}$$

$$\begin{array}{r} z^{-2} + 2z^{-1} + 1 \\ -z^{-2} + 3z^{-1} - 2 \\ \hline 5z^{-1} - 1 \end{array}$$

$$\Rightarrow X(z) = 2 + \frac{-1 + 5z^{-1}}{1 - \frac{3}{2}z^{-1} + \frac{1}{2}z^{-2}}$$

STEP 2: Factor denominator

ex.  $X(z) = z + \frac{-1 + 5z^{-1}}{1 - \frac{3}{2}z^{-1} + \frac{1}{2}z^{-2}}$

Factor:  $(1 - \frac{1}{2}z^{-1})(1 - z^{-1})$

$$X(z) = z + \frac{-1 + 5z^{-1}}{(1 - \frac{1}{2}z^{-1})(1 - z^{-1})}$$

STEP 3: Break  $X(z)$  into sum of factors of the form

$$\frac{A_k}{1 - d_k z^{-1}}, \quad \sum_{m=1}^S \frac{C_m}{(1 - d_k z^{-1})^m}$$

↑  
1st order  
(non-repeated)

↑  
S-th order pole  
(repeated S times)

\* re-learn how to deal with this \*

ex.  $X(z) = z + \frac{-1 + 5z^{-1}}{(1 - \frac{1}{2}z^{-1})(1 - z^{-1})}$

$$= z + \frac{A_1}{1 - \frac{1}{2}z^{-1}} + \frac{A_2}{1 - z^{-1}}$$



$$\frac{-1 + 5z^{-1}}{(1 - \frac{1}{2}z^{-1})(1 - z^{-1})} = \frac{A_1}{(1 - \frac{1}{2}z^{-1})} + \frac{A_2}{1 - z^{-1}}$$

$$= \frac{A_1(1 - z^{-1}) + A_2(1 - \frac{1}{2}z^{-1})}{(1 - \frac{1}{2}z^{-1})(1 - z^{-1})}$$

$$\Rightarrow -1 + 5z^{-1} = A_1(1 - z^{-1}) + A_2(1 - \frac{1}{2}z^{-1})$$

For  $A_1$ :  $z^{-1} = 2 \Rightarrow A_1(-1) = 9$

$$\boxed{A_1 = -9}$$

For  $A_2$ :  $z^{-1} = 1 \Rightarrow A_2(1 - \frac{1}{2}) = -1 + 5$

$$\boxed{A_2 = 8}$$

$$X(z) = 2 + \frac{-9}{(1 - \frac{1}{2}z^{-1})} + \frac{8}{1 - z^{-1}}$$

STEP 4: Invert, by inspection, each term (use tables)

$$\left\{ \begin{array}{l} \frac{1}{1 - az^{-1}}, \quad |z| > a, \quad \xleftrightarrow{z} a^n u[n] \\ \frac{1}{1 - az^{-1}}, \quad |z| < a, \quad \xleftrightarrow{z} -a^n u[-1-n] \end{array} \right.$$

(Note:  $\frac{1}{1 - az^{-1}} = \frac{z}{z - a}$ )

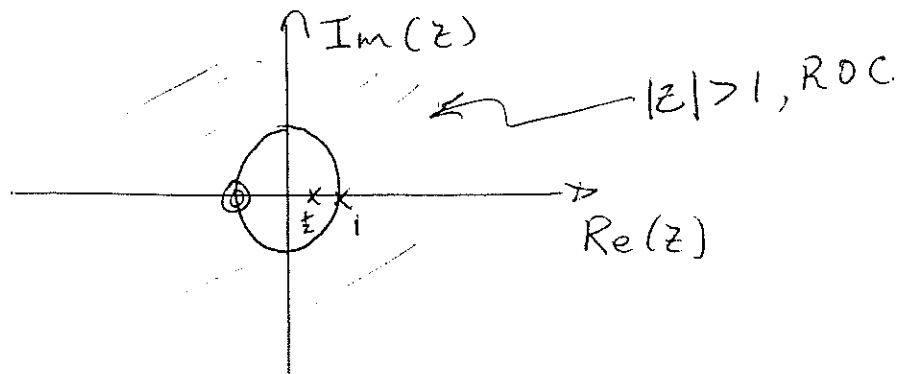
ex.  $X(z) = \frac{1 + 2z^{-1} + z^{-2}}{1 - \frac{3}{2}z^{-1} + \frac{1}{2}z^{-2}}, |z| > 1$

$$= z - \frac{4}{1 - \frac{1}{2}z^{-1}} + \frac{8}{1 - z^{-1}}$$

$\updownarrow z$                    $\updownarrow z$                    $\updownarrow z$

$$X[n] = 2\delta[n] - 8\left(\frac{1}{2}\right)^n u[n] + 8u[n]$$

Suppose  $|z| > 1$  was not specified. What other ROC's are possible?



Other possibilities:

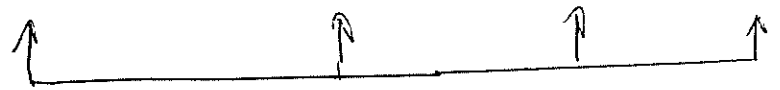
- (1)  $|z| < \frac{1}{2}$
- (2)  $\frac{1}{2} < |z| < 1$

What are the time-domain signals for (1) and (2)?

## (C) Power Series Expansion

$$X(z) = \sum_{n=-\infty}^{\infty} x[n] z^{-n}$$

$$= \dots x[-2] z^2 + x[-1] z + x[0] + x[1] z^{-1} + \dots$$



inverse transform comes up as coefficients of Laurent series expansion of  $X(z)$

★ Great for finite-length signals ★

ex.  $X(z) = z^2 (1 - \frac{1}{2} z^{-1})(1 + z^{-1})(1 - z^{-1})$

$$= z^2 - \frac{1}{2} z - 1 + \frac{1}{2} z^{-1}$$

$$x[n] = \delta[n+2] - \frac{1}{2} \delta[n+1] - \delta[n] + \frac{1}{2} \delta[n-1]$$

★ Useful when  $X(z)$  is not rational ★

ex  $X(z) = \log(1 + a z^{-1}) \quad |z| > |a|$

↪ complex logarithm

$$\log(1+x) = \sum_{n=1}^{\infty} \frac{(-1)^{n+1} x^n}{n}$$

$$X(z) = \sum_{n=1}^{\infty} \underbrace{\frac{(-1)^{n+1}}{n} a^n z^{-n}}_{X[n]}$$

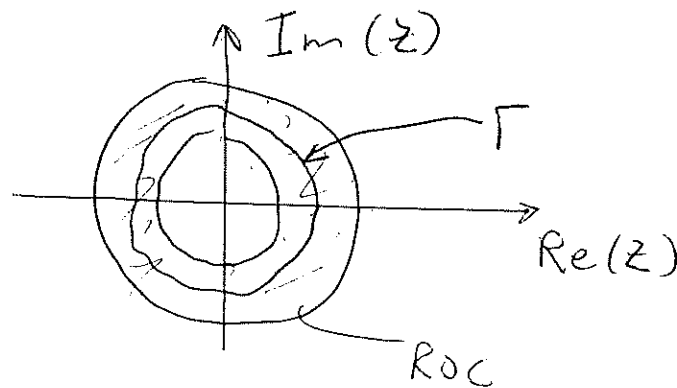
$$\Rightarrow X[n] = \begin{cases} \frac{(-1)^{n+1} a^n}{n}, & n \geq 1 \\ 0, & n \leq 0 \end{cases}$$

## ④ Inverse z-transform by Contour Integration

Without going into any details, we have

$$x[n] = \frac{1}{2\pi j} \oint_{\Gamma} X(z) z^{n-1} dz$$

Where  $\Gamma$  is a counter-clockwise contour in the ROC of  $X(z)$  encircling the origin of the z-plane



Requires knowledge of complex variable theory (Cauchy Residue Theorem)

For more details see

Digital Signal Processing  
by Oppenheim and Schaffer (1st edition)

p. 181-182

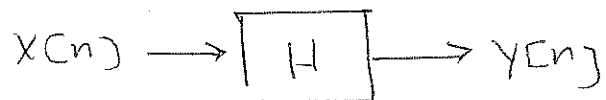
(if you're interested)

Z-transform  
Analysis of  
LTI Systems

# Analysis of DT systems and Filters Using the Z-Transform

Remember Difference Equations ?

Many LTI DT systems have input-output relationships that satisfy a linear constant-coefficient DE of the form:



$$\sum_{k=0}^N a_k Y[n-k] = \sum_{k=0}^M b_k X[n-k] \quad (1)$$

with zero initial conditions.

Take (1) to the z-domain by z-transform of both sides

$$\mathcal{Z} \left\{ \sum_{k=0}^N a_k Y[n-k] \right\} = \mathcal{Z} \left\{ \sum_{k=0}^M b_k X[n-k] \right\} \quad (2)$$

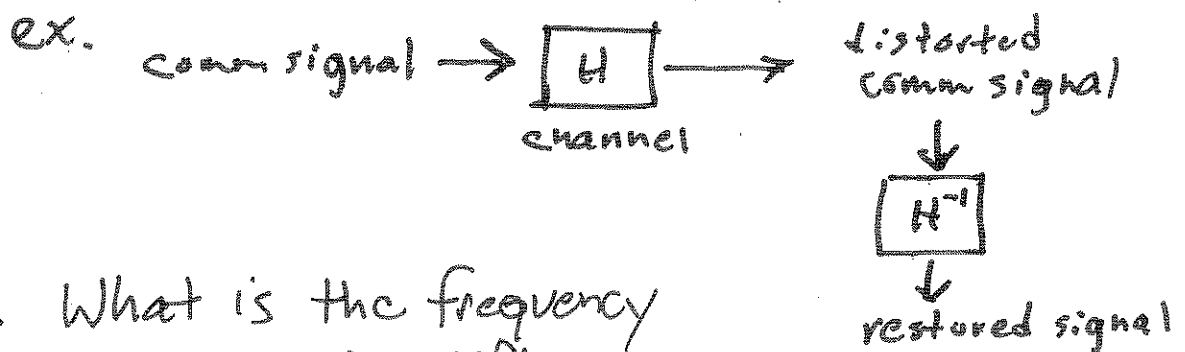
$$\text{Recall } X[n-k] \xleftrightarrow{\mathcal{Z}} z^{-k} X(z)$$

$\Rightarrow$

$$\sum_{k=0}^N a_k Y(z) z^{-k} = \sum_{k=0}^M b_k X(z) z^{-k} \quad (3)$$

## Questions:

1. When is a difference equation stable?
2. When is the corresponding impulse response / system causal?
3. Suppose the difference equation is a model for some system that we want to "undo". Does an "inverse system" exist.



4. What is the frequency response of a difference equation? How is it related to the z-transform?



$$(3) \Rightarrow \left( \sum_{k=0}^N a_k z^{-k} \right) Y(z) = \left( \sum_{k=0}^M b_k z^{-k} \right) X(z)$$

$$\Rightarrow H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^M b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

NOTES:

1.  $H(z)$  is a rational function !
2. Numerator coefficients come from RHS of (1).
3. Denominator coefficients come from LHS of (1).

Ex.  $x[n] \rightarrow \boxed{H} \rightarrow y[n]$

We are given an LTI system with transfer function

$$H(z) = \frac{(z+1)^2}{(z-\frac{1}{2})(z+\frac{3}{4})}$$

and wish to implement this system as an Linear constant-coeff. difference equation. What is the proper diff. eqn?

# ★★ STABILITY and CAUSALITY ★★

In going from

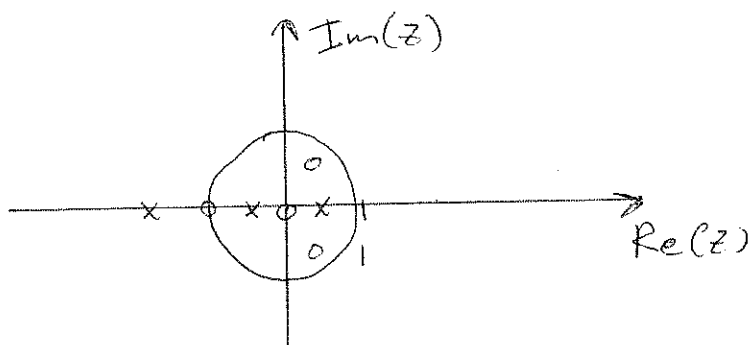
$$\sum_{k=0}^N a_k y(n-k) = \sum_{k=0}^m b_k x(n-k)$$

to

$$H(z) = \frac{Y(z)}{X(z)} = \frac{\sum_{k=0}^m b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}}$$

We did not specify an ROC.

If we factor  $H(z)$  into poles and zeros we can plot them in  $z$ -plane.



Several ROCs may be possible

- each ROC corresponds to a different impulse response
- which one to choose?

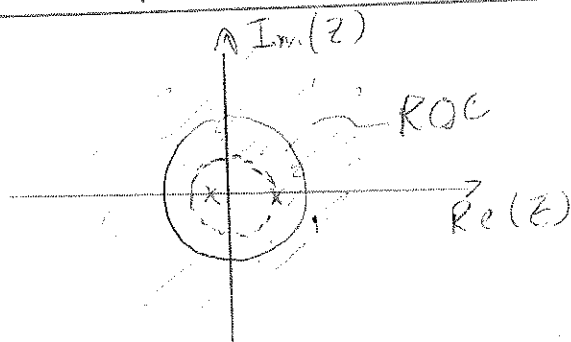
In general, there is no "right" choice:

However, there are some choices that make sense in practice.

### ★ Causality

$h[n]$  is causal if  $h[n] = 0, n < 0$

⇒ ROC extends outward from the outermost pole.



★ Stability A system  $\rightarrow \boxed{H} \rightarrow$  is  
BIBO stable

Note: 
$$|H(z)| = \left| \sum_{n=-\infty}^{\infty} h[n] z^{-n} \right|$$
$$\leq \sum_{n=-\infty}^{\infty} |h[n]| |z^{-n}|$$

On the unit circle, i.e.,  $\{ |z| = 1 \}$

$$\rightarrow |H(z)| \leq \sum_{n=-\infty}^{\infty} |h[n]|, \text{ for every } |z|=1$$

Therefore,

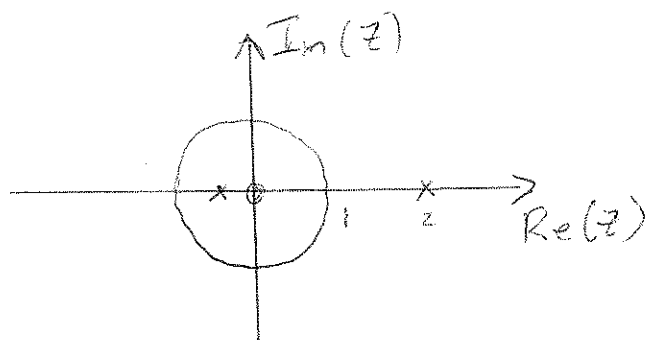
BIBO  $\iff$  ROC of  $H(z)$  includes the unit circle

## Key Questions:

Are stability and causality always compatible?

Ex. Consider

$$H(z) = \frac{z^2}{(z-2)(z+\frac{1}{2})}$$

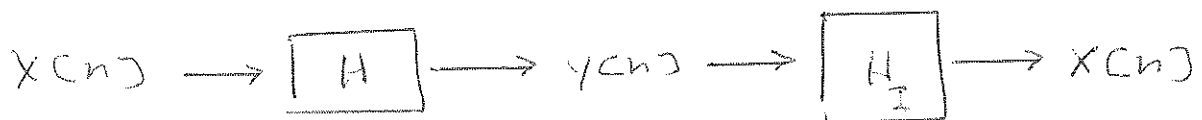


and its various ROCs and corresponding inverses  $h[n]$ .

## ★ INVERSE SYSTEMS ★



After passing  $x[n]$  through  $H$  to get  $y[n]$ , does there exist a system  $H_I$  that will give us  $x[n]$  back?



Obviously we need

$$H(z)H_I(z) = 1$$

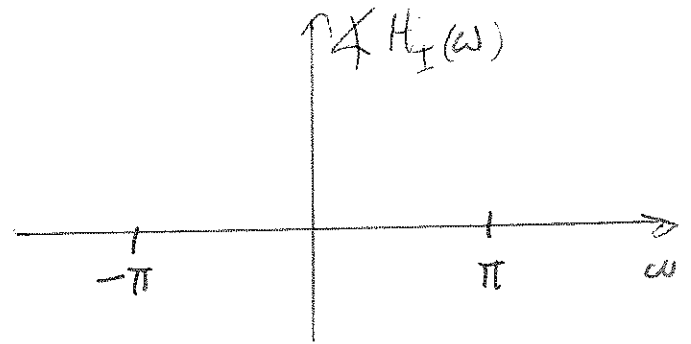
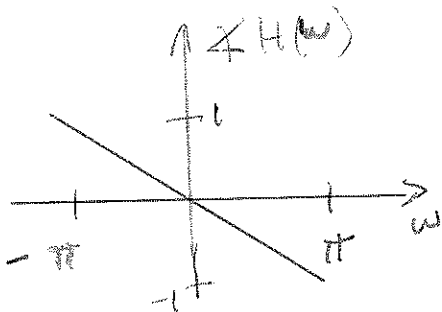
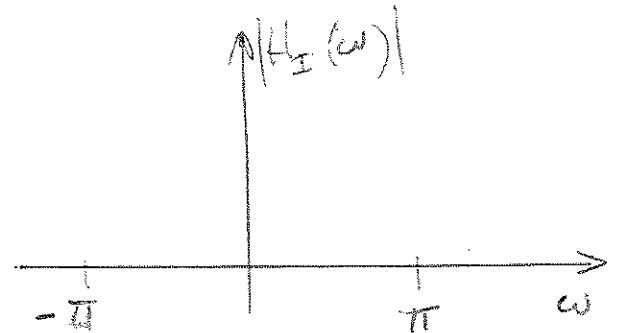
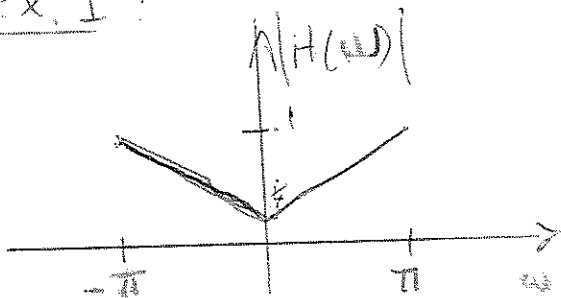
Equivalently in time domain:

$$h[n] * h_I[n] = \underline{\delta[n]}$$

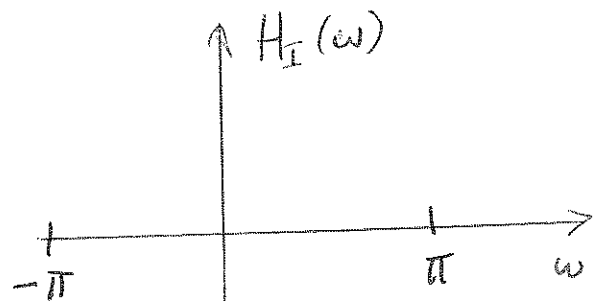
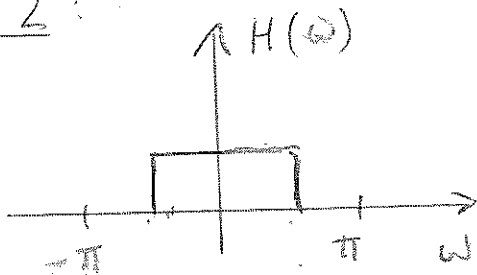
If  $H_I(z)$  exists, then its frequency response is

$$H_I(\omega) = \frac{1}{H(\omega)} \quad \left( \begin{array}{l} H(z) \text{ and} \\ H_I(z) \text{ evaluated} \\ \text{on unit circle} \end{array} \right)$$

Ex. 1:



Ex. 2:



Conclusion: Inverse of BIBO system exists if and only if  $|H(\omega)| > 0, -\pi < \omega < \pi$

Consider Rational  $H(z)$ .

$$H(z) = \frac{\sum_{k=0}^M b_k z^{-k}}{\sum_{k=0}^N a_k z^{-k}} = \frac{b_0}{a_0} \frac{\prod_{k=1}^M (1 - c_k z^{-1})}{\prod_{k=1}^N (1 - d_k z^{-1})}$$

$c_k$ 's are zeros of  $H(z)$

$d_k$ 's are poles of  $H(z)$

$$H_I(z) = \frac{1}{H(z)} = \frac{a_0}{b_0} \frac{\prod_{k=1}^N (1 - d_k z^{-1})}{\prod_{k=1}^M (1 - c_k z^{-1})} \quad \begin{array}{l} \text{poles?} \\ \text{zeros?} \end{array}$$

Question: What is the ROC of  $H_I$ ?

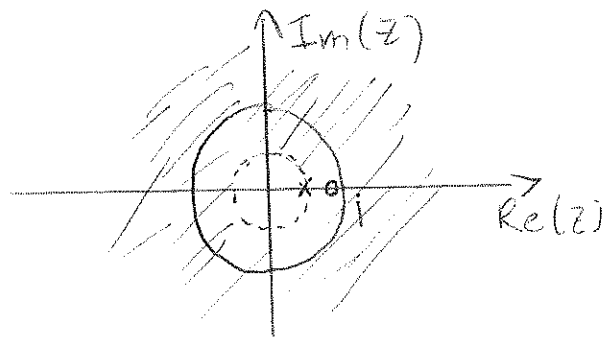
Recall  $H_I(z) = \frac{1}{H(z)} \iff \text{conv} \{h_I[n], h[n]\} = \delta[n]$

$\Downarrow$   
 ROC<sub>H</sub> and ROC<sub>H<sub>I</sub></sub>  
 must overlap

Ex.  $H(z) = \frac{1 - 0.5z^{-1}}{1 - 0.9z^{-1}}, |z| > 0.9$

Find  $H_I(z)$ , Is it stable? causal?  
and its ROC.

$$H_I(z) = \frac{1 - 0.9z^{-1}}{1 - 0.5z^{-1}}$$

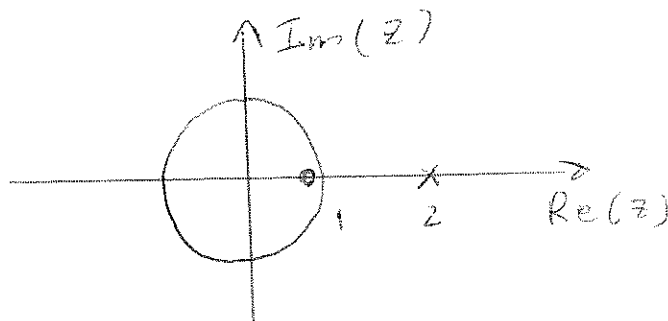


ROC:  $|z| > 0.5$  for causality

ROC includes unit circle  $\Rightarrow$  stability

Ex.  $H(z) = \frac{z^{-1} - 0.5}{1 - 0.9z^{-1}}, \quad |z| > 0.9$

$$H_I(z) = \frac{1 - 0.9z^{-1}}{z^{-1} - 0.5} = -z \left( \frac{1 - 0.9z^{-1}}{1 - 2z^{-1}} \right)$$



ROC:  $|z| > 2$  for Causality

$|z| < 2$  for stability

Conflicting requirements

Stable & Causal inverse does not exist!

(PROBLEM:  $H(z)$  has a zero outside the unit circle)

## Notes:

①  $H(z)$  stable, causal  $\iff$  poles inside unit circle

②  $H(z)$  has a stable, causal inverse  $H^{-1}(z)$   $\iff$  zeros of  $H(z)$  inside unit circle

① & ②

$H(z)$  stable & causal with stable, causal inverse  
if and only if

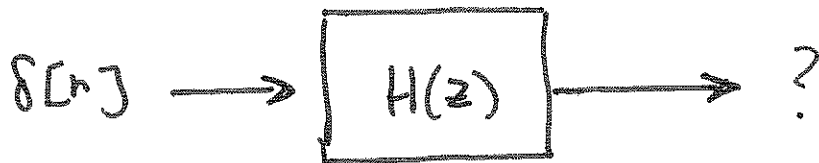
all poles and zeros of  $H(z)$  are inside the unit circle.

↙ This type of system is called a minimum phase system

★ Key in important applications



# Impulse Responses



$$H(z) = \frac{\sum_{k=1}^M b_k z^{-k}}{\sum_{k=1}^N a_k z^{-k}}$$

partial fraction expansion

$$H(z) = \sum_{r=0}^{M-N} B_r z^{-r} + \sum_{k=1}^{N_1-1} \frac{A_k}{(1-d_k z^{-k})} + \sum_{k=N_1}^{N_2} \frac{C_k d_k z^{-1}}{(1-d_k z^{-1})^2} + \dots$$

("non-repeated  
"1st order"  
poles
("repeated  
"second-order"  
poles

$\updownarrow z$

$$h[n] = \sum_{r=0}^{M-N} B_r \delta[n-r] + \sum_{k=1}^{N_1-1} A_k (d_k)^n u[n] + \sum_{k=N_1}^{N_2} C_k n (d_k)^n u[n] + \dots$$

\* Each pole contributes a term to the impulse response.

Ex.

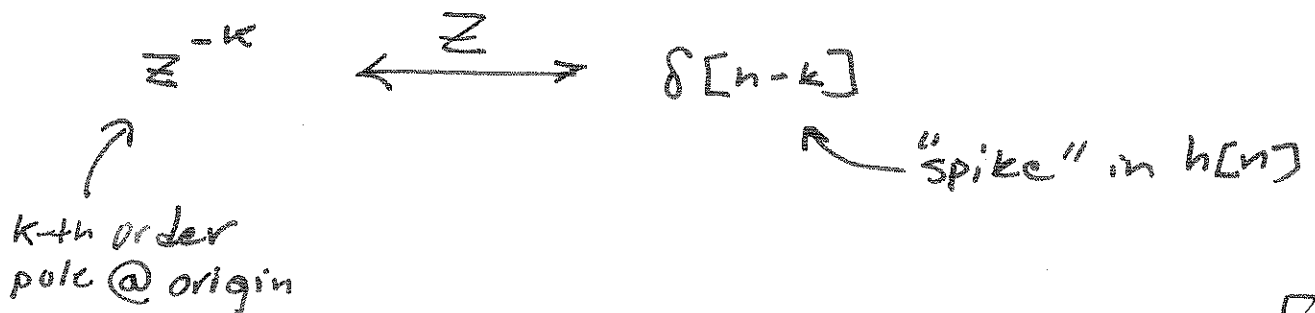
$$H(z) = z^{-1} + \frac{2}{1 - \frac{1}{2}z^{-1}} + \frac{\frac{1}{6}z^{-1}}{\left(1 + \frac{1}{3}z^{-1}\right)^2}$$



$$h[n] =$$

- 
- \* each pole has a contribution to impulse response
  - \* form of contribution depends on multiplicity of pole
  - \* Behavior of impulse response contribution depends on location of pole

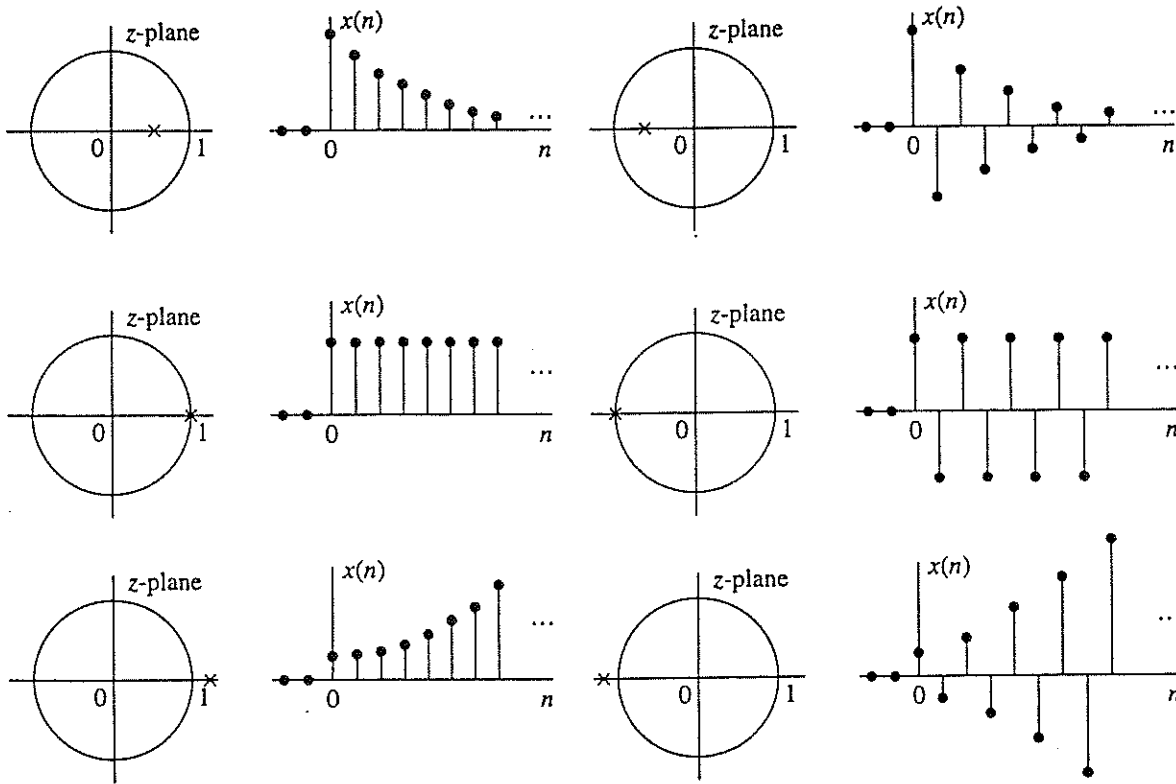
Simplest Case:



# Ex. Single Real Pole

$$\frac{z}{z-a} = \frac{1}{1-az^{-1}} \xleftrightarrow{z} a^n u[n]$$

$\nearrow$  pole @  $z=a$   
 ROC  $|z| > |a|$



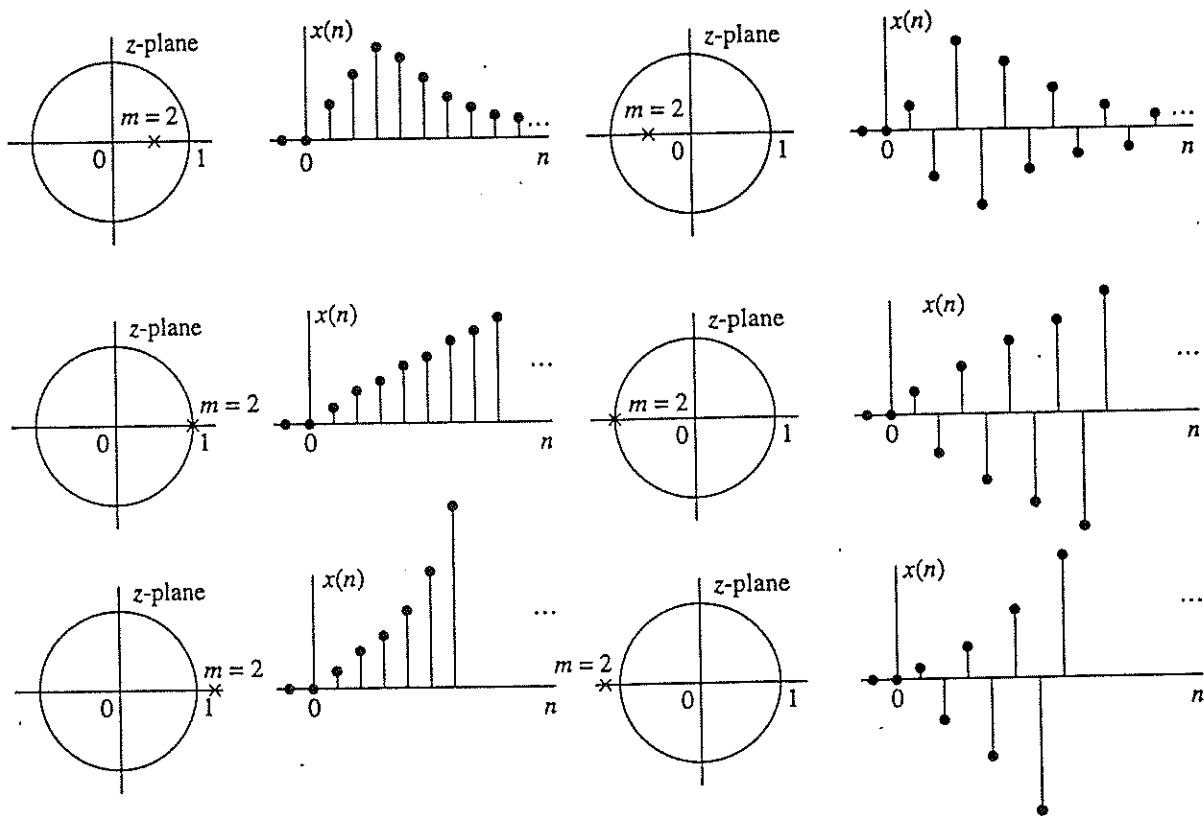
Figures on

from J. Proakis & D. Manolakis  
 "DSP", Prentice-Hall, 1995.

# Ex. Double Real Pole

$$\frac{az^{-1}}{(1-az^{-1})^2} \xleftrightarrow{Z} na^n u[n]$$

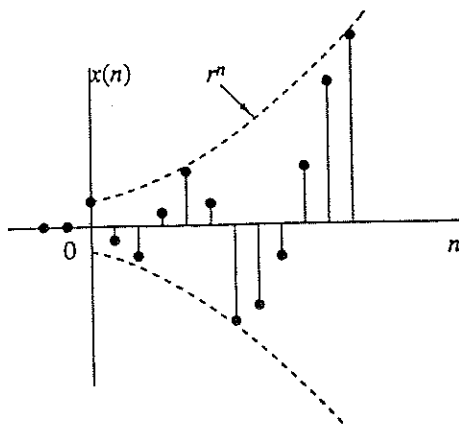
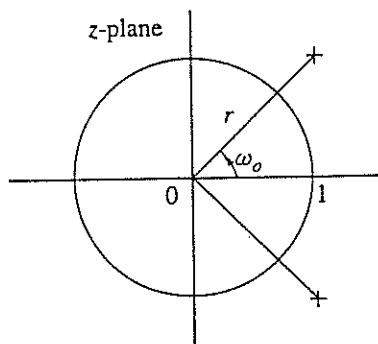
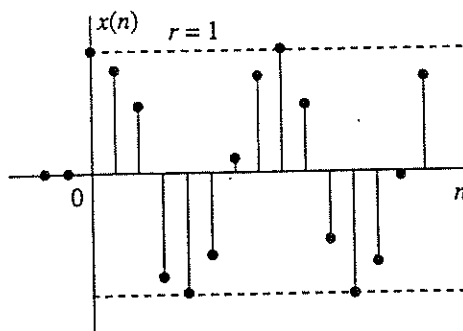
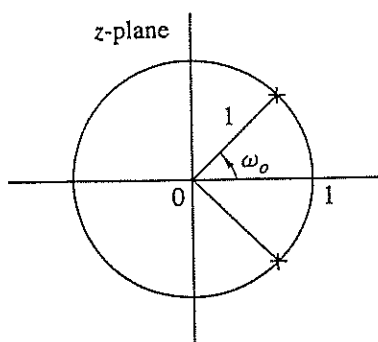
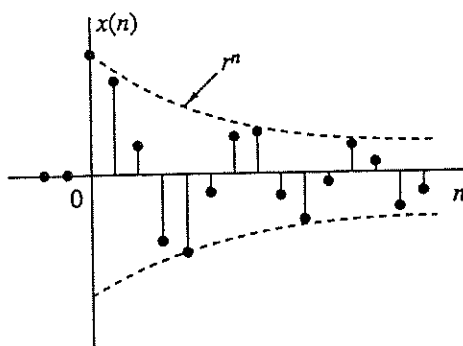
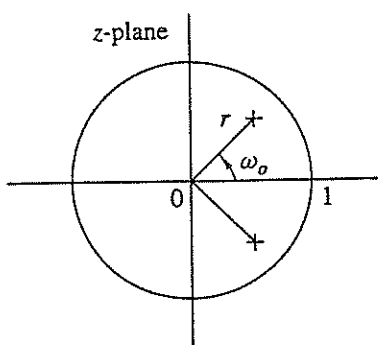
ROC  $|z| > |a|$



# Ex. Complex Pole Pairs

$$\frac{1 - (r \cos \omega_0) z^{-1}}{1 - (2r \cos \omega_0) z^{-1} + r^2 z^{-2}} \xleftrightarrow{Z} (\cos \omega_0 n) r^n u[n]$$

↑ poles @  $z = r e^{\pm j \omega_0}$



# Frequency Responses

How do poles and zeros influence the frequency response?

We will focus on the magnitude response. See OSB chapter 5 for examination of p

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Recall, BIBO stability condition  $\left(\sum_{n=-\infty}^{\infty} h[n] < \infty\right)$  implies that ROC of  $H(z)$  includes the unit circle. Therefore, the frequency response (DTFT) of  $h[n]$  is well-defined, and is given by

$$H(\omega) = H(z) \Big|_{z=e^{j\omega}} = \frac{\sum_{k=0}^M b_k e^{-j\omega k}}{\sum_{k=0}^N a_k e^{-j\omega k}}$$

We are going to look at  
 $|H(\omega)|$

the magnitude of the freq. response.

By factoring into poles and zeros, we have

$$H(\omega) = \frac{b_0}{a_0} \frac{\prod_{k=0}^M (1 - c_k e^{-j\omega})}{\prod_{k=0}^N (1 - d_k e^{-j\omega})}$$

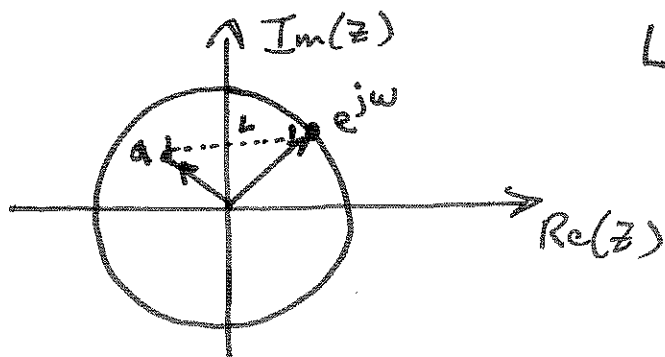
and thus

$$|H(\omega)| = \left| \frac{b_0}{a_0} \right| \frac{\prod_{k=0}^M |1 - c_k e^{-j\omega}|}{\prod_{k=0}^N |1 - d_k e^{-j\omega}|}$$

Next, multiply by  $\frac{|e^{j\omega}|^M}{|e^{j\omega}|^N} = 1$  to get

$$|H(\omega)| = \left| \frac{b_0}{a_0} \right| \frac{\prod_{k=0}^M |e^{j\omega} - c_k|}{\prod_{k=0}^N |e^{j\omega} - d_k|}$$

What is  $|e^{j\omega} - a|$ ?



$L = |e^{j\omega} - a|$  = length of vector connecting  $e^{j\omega}$  and  $a$

$$|H(\omega)| = \left| \frac{b_0}{a_0} \right| \cdot \frac{\prod_{k=0}^M |e^{j\omega} - c_k|}{\prod_{k=0}^N |e^{j\omega} - d_k|}$$

- $c_k$  - zero  $\Rightarrow |e^{j\omega} - c_k| =$  distance from  $e^{j\omega}$  to  $c_k$

$\Rightarrow$  numerator consists of the product of the distances from  $e^{j\omega}$  to all zeros of  $H(z)$

- $d_k$  - pole  $\Rightarrow |e^{j\omega} - d_k| =$  distance from  $e^{j\omega}$  to  $d_k$

$\Rightarrow$  denominator of  $|H(\omega)|$  consists of product of the distances from  $e^{j\omega}$  to all poles of  $H(z)$ .

- overall magnitude of frequency response @  $\omega$

$$|H(\omega)| = \frac{\prod \text{"distances from zeros"}}{\prod \text{"distances from poles"}} \cdot \left| \frac{b_0}{a_0} \right|$$

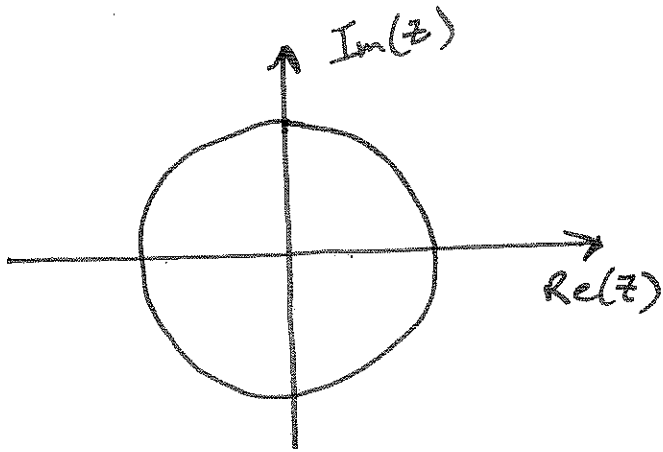
Therefore,

Close to a zero  $\Rightarrow$  magnitude is \_\_\_\_\_

Close to a pole  $\Rightarrow$  magnitude is \_\_\_\_\_



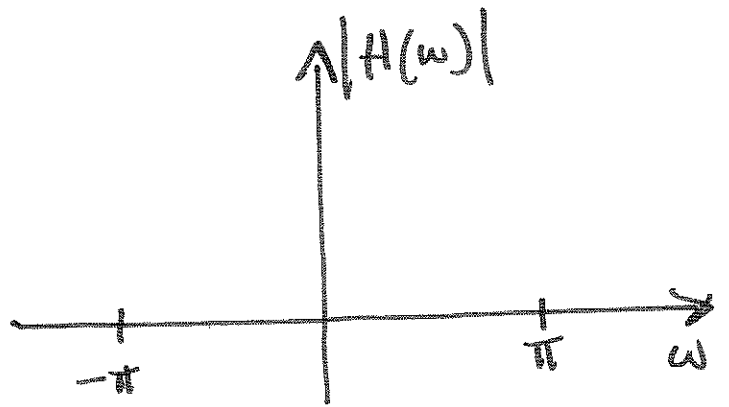
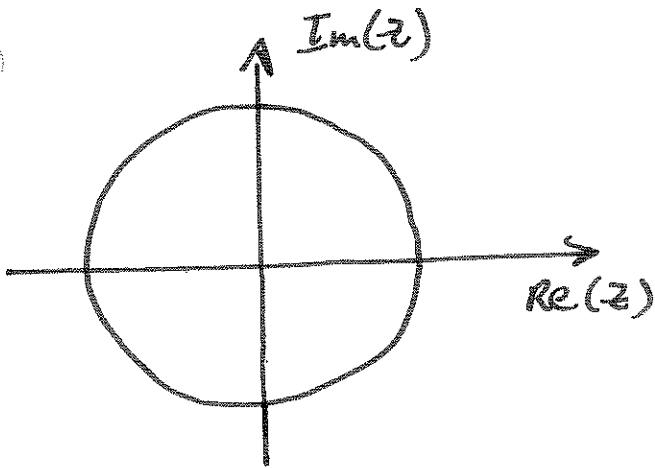
Ex.  $H(z) = z^{-1}$ , ROC  $|z| > 0$ , pole @ 0  
zero @  $\pm\infty$



$$|H(\omega)| =$$

Ex.  $H(z) = \frac{z}{z - \frac{1}{2}} = \frac{1}{1 - z^{-1} \frac{1}{2}}$ , ROC  $|z| > \frac{1}{2}$

zero:  $z = 0$   
pole:  $z = \frac{1}{2}$



$$|H(\omega)|^2 =$$

Ex. Plot  $|H(\omega)|$  corresponding to  
the pole-zero plot

